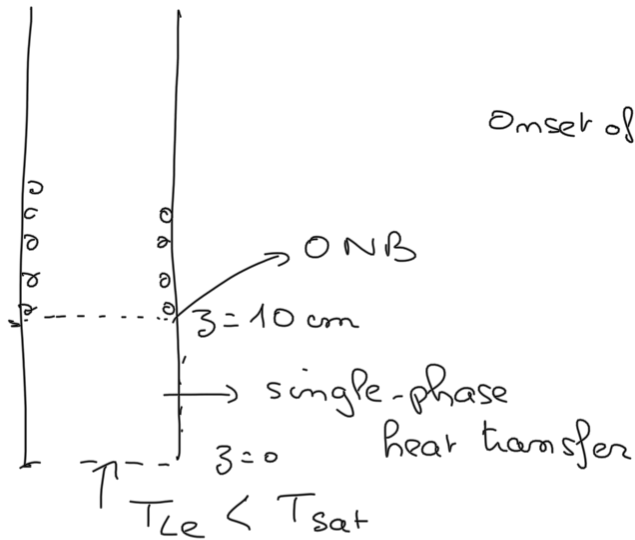


Exercise 1



$$T_p = 281^\circ\text{C}$$

ONB if $T_p - T_{\text{sat}} > \left[\frac{8 \sigma T_{\text{sat}} q_{\text{ONB}}}{\lambda_L \rho_L h_{\text{LV}}} \right]^{1/2} \frac{1}{Pr_L}$

Onset of Nucleate Boiling

$$q_{\text{ONB}} < \frac{\lambda_L \rho_L h_{\text{LV}}}{8 \sigma T_{\text{sat}}} \left[Pr_L (T_p - T_{\text{sat}}) \right]^2$$

In single-phase liquid flow

$$q_p = h (T_p - T_L(z))$$

$$Nu = \frac{hD}{\lambda_L} = 0.023 Re^{0.8} Pr^{1/3}$$

$$\pi D q_p = \pi D h (T_p - T_L(z)) = \underbrace{GA}_{\dot{m}} c_p \frac{dT_L}{dz}$$

$$q_{\text{ONB}} = 4.3 \text{ MW/m}^2$$

$$\frac{dT_L}{T_p - T_L} = \frac{h \pi D}{GA c_p} dz = \frac{4h}{DG c_p} dz$$

$$\frac{dT_L}{T_p - T_L} = \frac{4h}{DG c_p} dz \quad \hookrightarrow \quad \frac{T_p - T_L}{T_p - T_{\text{Le}}} = e^{-\frac{4h z}{DG c_p}}$$

$$q_p = h (T_p - T_L) = h (T_p - T_{\text{Le}}) e^{-\frac{4h z}{DG c_p}}$$

$$q_p(z=0.1\text{m}) = q_{\text{ONB}} \rightarrow T_p - T_{\text{Le}} = \frac{q_{\text{ONB}}}{h e^{-\frac{4h z}{DG c_p}}}$$

$$Re_L = \frac{GD}{\mu_L} = 907258$$

$$Nu = 1282$$

$$h = 74464 \text{ W/m}^2/\text{K}$$

$$T_p - T_{\text{Le}} = 61.64^\circ\text{C}$$

$$T_{\text{Le}} = 219.36^\circ\text{C}$$

$$T_{\text{sat}} - T_{\text{Le}} = 277 - 219.36 = 57.64^\circ\text{C}$$

Exercise 2

Ethanol $\rightarrow 50^\circ\text{C} = T_L$

$$T_{\text{sat}} = 100^\circ\text{C}$$

$$T_p = 140^\circ\text{C}$$

$$q = q_m + q_e = H(T_p - T_L)$$

$$T_L = T_L(z)$$

boiling

convection in the liquid

$$q_m = \mu_L h_{LV} \left[\frac{g(\rho_L - \rho_V)}{\sigma} \right]^{1/2} Pr^{-5} \left[\frac{C_p(T_p - T_{sat})}{0.013 h_{LV}} \right]^3 = 16957 \text{ W/m}^2$$

$$q_e = h_e (T_p - T_L) \quad Nu = \frac{h_e D}{\lambda_L} = 0.023 Re^{0.8} Pr^{1/3}$$

$$h_e = 1693 \text{ W/m}^2/\text{K} \quad Re = \frac{GD}{\mu_L} = 22930$$

$$H = \frac{q_m + q_e}{T_p - T_L} = h_e + \frac{q_m}{T_p - T_L} = 2034 \text{ W/m}^2/\text{K}$$

\downarrow \downarrow
 1693 \quad ≈ 300 (\uparrow of 20% due to boiling).

To calculate the evolution of liquid temperature $T_L(z)$

$$G C_p \frac{dT_L(z)}{dz} = \frac{4 q_p}{D} = \frac{4}{D} (q_m + h_e (T_p - T_L))$$

$$\frac{dT_L}{\frac{q_m}{h_e} + T_p - T_L} = \frac{4 h_e}{D G C_p} dz \Rightarrow \frac{q_m}{h_e} + T_p - T_L = \left(\frac{q_m}{h_e} + T_p - T_{le} \right) \times e^{-\frac{4 h_e z}{D G C_p}}$$

$$T_L(z) = 90^\circ\text{C} \quad \text{for } z = 1.85 \text{ m}$$

Exercice 3 = Comparison of the correlations of

Kandlikar and Gungor and Winterton

Nitrogen $x = 0.2$ $x = 0.6$

Gungor and Winterton

$$H = h_L \left[1 + 3000 Bo^{0.86} + \left(\frac{x}{1-x} \right)^{3/4} \left(\frac{\rho_L}{\rho_g} \right)^{0.41} \right]$$

$$Bo = \frac{g}{G h_{LV}} = 6.17 \cdot 10^{-4} \quad h_L = 0.023 \frac{\lambda_L}{D} \left(\frac{G(1-x)D}{\mu_L} \right)^{0.8} Pr^{1/3}$$

$$\text{For } x = 0.2 \quad h_L = 742 \text{ W/m}^2/\text{K}$$

$$H_{Gw} = 5528 \text{ W/m}^2/\text{K}$$

$$\text{For } x = 0.6 \quad h_L = 425 \text{ W/m}^2/\text{K}$$

$$H_{Gw} = 4666 \text{ W/m}^2/\text{K}$$

Kandlikar

$$H = h_L \left[C_1 C_0^{C_2} + C_3 Bo^{C_4} Fr_K \right] \quad Fr_K = 4.70$$

$$x = 0.2$$

$$C_0 = \left(\frac{1-x}{x} \right)^{0.8} \sqrt{\frac{\rho_g}{\rho_l}} = 0.652 > 0.65 \rightarrow \text{nucleate boiling regime}$$

$$C_1 = 0.6683$$

$$C_2 = -0.2$$

$$C_3 = 1058$$

$$C_4 = 0.7$$

$$H_k: 21360 \text{ W/m}^2/\text{K}$$

$$x = 0.6$$

$$C_0 = 0.155 < 0.65 \rightarrow \text{convective boiling regime}$$

$$C_1 = 1.1360$$

$$C_2 = -0.9$$

$$C_3 = 667.2$$

$$C_4 = 0.7$$

$$H_k(0.6) = 10125 \text{ W/m}^2/\text{K}$$

